## Europa Gross Weight Increase An Analytical Approach

By Bud Yerly

While working at Flight Crafters I was part of the conversation on the Gross Weight Increase for the Europa.

The problem with most light aircraft is the aircraft design and the prototype were around a payload of 500 pounds maximum. However, most pilots and passengers are no longer 170 pounds each and fuel loads and payloads are always increasing. Worst yet, the aircraft undergoes mission creep. The designer proposed a light VFR aircraft with minimal equipment, no interior beyond a cushion, a small engine and fixed wood propeller. However, the builder (and the dealers) tend to load up the aircraft to meet the demands of the prospective buyer.

Buyers want all the doodads and bells and whistles, a comfy cushion, for their turbocharged engine, constant speed propeller, oxygen tanks for high altitude cruise, autopilots, external lighting, additional alternators, batteries for backup, additional fuel tanks, and a larger fully packed instrument panel completely packed with every instrument known to man. So the light weight 800 pound prototype grows to an 1100 pound empty weight experimental. However, the maximum gross weight stays at 1300 pounds.

Europa aircraft realized this and improved the structure, and maximum gross weight with Mod 52 to 1370. Unfortunately, even that wasn't enough.

In the US and other countries requests were made to Europa Aircraft to increase the maximum gross even higher. Andy Draper in emails and faxes commented that since the Europa was built with a superfactor (a load factor of 1.5 over the design G limit is standard as a maximum G load which the aircraft must demonstrate for 3 seconds prior to breakup, but the Europa was designed to a 1.5 times 1.5 safety factor or superfactor). This superfactor was to be an additional pad for amateur building errors. Essentially the 3.8 G standard maximum G for the Europa made for a design that is overly strong and the major wing and fuselage structure were designed and demonstrated at the following: 3.8 positive G X 1.5 X 1.5 which yielded a structure able to achieve 8.55 Gs if for only a moment for breakup.

This superfactor means one of two things. The aircraft gross weight can be increased or you can pull more Gs. But that is not sane. An increase in gross weight affects many other things also.

The stall speed will increase slightly, the CG range has to be tightened up for longitudinal stability, the tail force will be the same but its affect on the ability to raise the nose for the flare at the forward CG is significantly different. Landing gear attach points must be retested for heavier landing weight. Spin characteristics with different heavier loadings must be evaluated.

A heavier aircraft will have a longer takeoff and landing roll which must be computed, climb rate will be lower, with lower climb rates the aircraft will take longer to get to altitude and the engine will be stressed longer, cruise speeds will be lower due to a higher angle of attack at cruise. Final approach speed will be slightly higher, but the sink rate power off in a glide will be higher as will the sink rate on final requiring a bit more power on approach increasing residual thrust in the flare increasing landing roll. Wheels and brakes will be taxed more. All this additional testing will also have to be approved in the UK and other countries. Flight and ground stress tests must be done at significant cost. Pilot handbooks will need to be modified. As a result, Europa Aircraft never pursued this gross weight increase.

When I began Custom Flight Creations in the USA, the FAA does not consider a change in GW to be a problem. The kit builder (an amateur) can make the change as in the US the kit manufacturer is only a component manufacturer and the builder is considered the manufacturer. It is beyond the scope of this paper to determine whether this is a smart policy.

At Custom Flight Creations, I went about the analytic and flight testing to see if a 1450 pound maximum takeoff weight was sane and rational. In my analysis I took a different option than simply assuming the structure superfactor would protect me and my clients. I also kept the maximum landing weight at 1370 pounds to keep landing gear and landing characteristics the same for the GA pilot flying the Europa.

In my analysis I reduce the maximum load factor in proportion to the GW increase. This allows the superfactor to still be present even at the higher weight. Of course all the other factors with the GW increase will still be a factor and must be analyzed and computed changes made.

The calculations are attached at the end of this document. To summarize:

Maximum takeoff weight (MTOW) to 1450 pounds XS or Classic aircraft. VEAS is within instrument tollerances if the pitot tube is placed IAW the XS manual. Maximum Landing weight is maintained at 1370 pounds.

Aircraft G limit change at 1450 pounds +3.59 , -1.79

- Vne: 165 KIAS for XS, 160 Classic.
- Va: 96 KIAS
- Vno: 125 KIAS based on updated gust load factors.
- Vfe:
   83 KIAS

   Vso:
   50 KIAS

   Vsf:
   45 KIAS
- Vx: 61 KIAS
- Vy: 75 KIAS
- VI/d: 75 KIAS

Takeoff Roll: 750 feet sea level standard day.

Landing Roll: 750 feet full flap, maximum braking no wind 1450 pound over gross landing. Rate of Climb, constant speed propeller or fixed climb prop: 914: 900fpm, 912S: 650fpm, 912: 500fpm Due to longer climb consider a 80-90 KIAS climb speed to enhance cooling.

Attached:

- 1. Europa GW increase considerations.xlsx
- 2. VN Diagrams.xlsx
- 3. Europa Aircraft Tech Andy Draper MTOW increase Fax discussion.

## Attachment 1.

Europa Gr	oss Weigh	lncrease l	Data N12A	for the p	ossibility o	of an increa	ase								
in the GW	to 1450 lb:	5.		•											
The increa	se in Gros	Weight (	GW) requir	es more th	nan just an	arbitrary c	hange to t	he GW limi	it						
posted in	the Europa	Pilots Har	ndbook of 1	370 lbs.											
Considera	tions:														
	Increasing	the GW fr	om 1370 to	1450 MTC	W analyti	cally calcul	ated.								
	Maximum	ultimate s	trength												
		No ultima	te strength	changes a	are conside	ered.									
		No ultima	te load tes	ts are to b	e conducte	ed.									
		This is an a	analytic exe	ercise.											
Current De	esign Load	Limit.													
	3.8 G at 13	70 lbs. Fro	m CG of 58	-62.5 inch	es.										
Over Gros	s Limit Cha	nges Cons	idered for	This Exerc	ise.										
	MTOW inc	rease to 14	450 lbs allo	ws full fue	el and take	off only.									
	Maximum	Landing W	/eight will	remain at	1370 lbs.										
	Landing ov	/er 1370 lb	s will requi	re a hard l	anding ov	er load lan	ding inspe	ction.							
Adjusted (	Gross Weig	ht (AGW)													
	The AGW	of 1450 lbs	increases 1	the GW by	80 lbs.										
	The Maxin	num G Lim	it is adjuste	ed as follo	WS:										
	1370	is	X		X is the A	djusted G L	.imit								
	1450	to	3.8		X equals	3.59	Positive G	limit							
	2 50 6	م الع	:						1						
	3.59 GS WI	limite are	e aircraft to	structura	lly fly at lo	w speed w	Negative	iperractor i	imits.						
CClimitat	ions with (		the locroper	1150.		1.79	Negative	Ginnit							
CGLIIIItat	Elight tost	indicatos t	that the for	:. ward limi	t for full fl	an landing	is limited	to 50 incho	s ( G						
	At 58 inch	s and 13 d	legrees of I	E down o	f the stah	harely allo	ws the air	craft to flar	e out now	eroff					
	No affect (	n stall nit	tch stahility	or spin re	covery (or	ne turn) oc	curs at 62	5 however	the Triges	ar					
	landing ge	ar position	without n	ilots in th	e aircraft a	llows the a	aircraft eas	ilv he nusł	ed on its t	ail					
	An aft limi	t of 62 incl	nes allows	the aircraf	t to not fa	ll on its tail	l and stay t	here for lo	ading and	eround hai	ndling				
	At 62 inch	es the aircr	raft was sta	lled fully	and cross o	controlled	to enter a s	spin. Reco	verv was in	nmediate.					
	The aircra	t is still lo	ngitudinall	v stable at	a CG of 62	.5 inches.	but with fu	III baggage	and fuel w	ith no pilo	ts, the plar	es CG is v	erv close to	the main	gear.
								30-3-			, . p		,		-
VN change	es with inci	ease in Gr	oss Weight												
	During cru	ise in verti	ical gust co	nditions tl	ne aircraft	may excee	d its G lim	its inadver	tantly.						
	However,	at speeds	below app	roximatel	125 KIAS	a vertical g	ust may st	all the airc	raft at low	speed					
	before the	load facto	or is exceed	ded.											
Landing ge	ear compor	nent streng	gth conside	rations:											
	Wheels	Matco Mfg	g. WHL 51 n	ormal loa	d min 1200	), maximun	n load 3600	per whee	Ι.						
	Gear legs	RV4 desig	n based on	load of 15	50 lbs. nor	mal max lo	oad. These	are the le	gs used ori	ginally on	the Europa	Trigear.			
		Manufactu	urer of the	se gear leg	s was: Lar	ngair Machi	ning Inc.								
	Gear leg a	ttachment	points: Af	ter 10 yea	rs of flying	and landir	ng overgro	ss Europa a	ircraft at o	r near 1450	) lbs withou	it ever			
	bending a	gear leg or	r causing a	deformati	on of the g	gear box, it	seems str	ong enoug	h. Analytic	ally, the g	ear box 3/4	ply compr	ression		
	capability	with the g	lass, excee	ds a 4 G in	npact load	at 1370 lbs	with the g	gear as des	igned.						
	(Based on	a 33 inch le	eg, 3/4 mar	ine ply, ar	nd a max lo	bad at land	ing of 2900	) lbs per tir	e. Lestima	te a <b>4 G</b> in	npact will st	ill allow a	nother 30%	6 safety fa	ctor.
	The steel s	leeve and	bolt holdi	ng the gea	r however	may begir	n to elonga	te which is	s difficult to	o repair.					

## Attachment 1 contd.

		-													
Suggeste	d Placard Fo	or MTOW o	of 1450 lbs.												
	G Limit 3.8	3 Gs at 1370	) lbs, CG 58	-62.5 inche	S										
	G Limit 3.5	5 Gs at 1450	) lbs, CG 59	-62 inches											
	Maximum	Landing W	/eight 1370	) lbs in all c	ases.										
	Landings a	bove 1370	lbs may b	e accompli	shed provi	ded an									
	inspectior	n of the gea	ar is accom	plished.											
Suggeste	d over gros	s landing g	ear checkli	st:											
	Fuselage	Area													
	Mono:														
	•	Fuselage	through bol	t attachmer	ts of the m	iain gear w	elded frame	e bolts and	holes for ele	ongation/ d	eformation	or de-lamin	ation.		
	•	Landing g	ear and en	gine mount	trame for o	leflections,	cracks or c	out of alignn	hent conditi	on.					
	•	Cockpit m	nodule whee	el well for de	eformation	s, puncture	s or de-lam	inations.							
	•	Inspect al	Redux/Ara	aldite 420A/	B joints via	a tap metho	d for hollov	v sound ind	icating de-la	amination o	r failed joir	nts.			
	•	Check the	belly sides	and top fo	r wrinkles	or deforma	tions in the	fuselage.							
	•	Wing atta	chment and	lift pin for	deformatio	ns.			<u> </u>						
	•	check the	LG04 pin f	or straightn	ess and all	the mount	ng and swii	ng hardware	e for deform	nations, loo	seness or o	racks, meci	nanısms.		
			Pay particu	ilar attentio	n to the up	and down	lock								
	•	Inspect th	e wheel for	cracks and	damage.		de le colores								
	•	Rear fuse	lage emper	lage for der	ormations/	wrinkles or	de-laminat	ions.							
	•	Inspect th	e tail sprin	g attachmer	t bolt and	mount for s	straightness	, deformati	ons or elong	gations.					
			Inspect th	e spring for	straightne	ss and crac	ks as well a	as security.							
		Europeiro I	Inspect the	wheel fork	and bearing	gs for defori	mations or a	abnormalitie	es. Inspect t	he wheel an	d tire.				
	•	Examine t	the wing att	achments a		ers for deto	rmations a	nd cracks a	s in the Ove	er G inspect	ion.				
	•	Examine t	the landing	gear frame	for cracks	or deforma	ation in the	frame, ove	Center lock	and compo	onents.				
	Trigopri														
	mgear.	in Londing (	Coor Aroos												
	Pid	in Lanung (	by the tail (	ufficient to	chack tha	noor for loc	COROCC								
		Increat th	o aircraft f	or wheel to	in and ali	anment Th	are should	be zero tor	with weigh	t off the wh	) Deels				
		Inspect th	e tracking	with weight	on the whe	ale		De 2010 100	e with weigh		10013.				
	•	lack the a	aircraft and	check the le	eq for crac	ks. deforma	ation, and t	he spindle a	nd wheels f	for damage					
		Check the	tire(s) for	wear, cuts	and flat sp	ots.				a aanage					
	•	Inspect th	e wheel for	cracks and	damage.										
		Check the	wheel pan	ts and brac	kets for cra	acks and de	formations								
		inspect the	e nose gear	leg bolts a	nd welds fo	or deformat	ions, crack	s or misalio	nment, Ch	eck the pive	ot bushinas	for wear an	nd soundne	ss.	
			Check the	bump stop	and leg for	any deform	ation								
		Check the	engine mo	unts, gear	frame and	supports fo	r cracks, el	longated bo	lts or defori	nations.					
	1						, -								

## Attachment 2

	Efford	to of C		aight In		o from	1270	+0 140										
	Lilec		055 99	eignun	ici eas	enom	13/0	10 14.	50 105.									
Addeduur	alaht ingraa	cos stall sos	od Indicate	d holow the	Incrosco	of 90 lbc role	oc stall spa	od hu on o	knot									
Added we	eight increa	ises stall spe	ed. Indicate	to below, the	e increase o	or 80 lbs rais	es stall spe	ed by one	knot.									
	GW	Stall Speed	Nominal G	Negative G														
	1450	50	3.6	-1.8														
	1370	49	3.8	-1.9														
	1100	45	3.05	-2.35														
	0	0	0	0														
The veloc	ty vs G loa	ding of the a	ircraft are af	fected also.														
		1270 LE CIV		AAFOLIN CHA														
	V	N N	V	1450 LD GVV														
	160	3.8	160	36														
	150	3.8	150	3.6														
	140	3.8	140	3.6														
	130	3.8	130	3.6														
	120	3.8	120	3.6														
	100	3.8	100	3.6														
	95	3.8	96	3.6														
	84	3	87	3														
	69	2	/1	2														
	49	03	28	03														
	10	0.05	11	0.05														
	0	0	0	0														
	10	-0.05	12	-0.05														
	25	-0.29	29	-0.3														
	50	-1	52	-1														
	70	-1.9	67	-1.8														
	100	-1.9	100	-1.8														
	120	-1.9	120	-1.8														
	140	-1.9	140	-1.8														
	150	-1.9	150	-1.8														
	160	-1.9	160	-1.8														
Gust facto	or on G load	ling:																
	A strong 5	0 tps or 3000	fpm up/dov	vndraft verti	cal gust (at	oout 39 Knot	s)					Veas KTS	Ve tps	Vgust tps	Delta CL	Vd		
	affects the	maneuverir	inicantiy, an	) of the aircr	aft and the	max structu	ering of the	sneed (Vr	20)			50	84	50	stall			
	green arc	or rough air	limit should	be adjusted.				speed(vi				75	126	50	stall			
												100	168	50	16.6			
	A crude bu	ut effective i	method is to	use the delt	a lift by the	e gust factor	on the lift	curve slope	e.			125	210	50	13			
	Then calcu	late the equ	uivalent airs	peed decreas	se for that	load and plo	t on the cu	rve below:										
	n= 1 : (Ka)	lauct V n C/	2147)	Va= 00/E 3		u= 2m/n C a	C whore a	is the cont	trifical accoloration			U 44.60	Kg 0.79	n 171	@ 1270 an	d E0 fec		
	11= 11 (Kg )	igust v p 5/2		Ng=.000/ J.J		u= zni, p c a	15 where a	is the cent				44.69	0.78	1.71	@1370 and	d 66 fps		
		1370 Lb	s. 50 fps	1	1450 LI	bs. 66fps	1											
		A/S	Gust Factor		A/S	Gust Factor												
		0	1		0	1												
	A rough of	125	2.78	uld he cheng	125	2.87	125 1/145											
	A rough a	i penetratio	ii speeu siio	uiu be chang	eusiigiiuy	110111 151 10	125 KIAS										 	
													AS	Gust Facto	or			
	Based on 3	100 sq ft win	g area flaps	up.									AS 0	Gust Facto	or 0	1		
	Based on 2 Cl of 1.67	100 sq ft win clean wing	g area flaps	up.									AS 0 125	Gust Factor 1 2.78	or 0 125	1		
	Based on 1 Cl of 1.67	100 sq ft win clean wing	g area flaps	up.									AS 0 125	Gust Facto 1 2.78	or 0 125	1 2.87		
	Based on 1 Cl of 1.67	100 sq ft win clean wing Eu	g area flaps	up. Classic	: V/N D	iagram	Calcula	ated					AS 0 125	Gust Facto 1 2.78	or 0 125	1 2.87		
	Based on 2 Cl of 1.67	100 sq ft win clean wing Eu	g area flaps	up. Classic	: V/N D	iagram	Calcula	ated					AS 0 125	Gust Facto 1 2.78	or 0 125	1 2.87		
	Based on : Cl of 1.67 (	100 sq ft win clean wing Eu	g area flaps	<sup>up.</sup> /Classic	: V/N D	liagram	Calcula	ated					AS 0 125	Gust Factor 1 2.78	or 0 125	1 2.87		
5	Based on 2 Cl of 1.67	100 sq ft win clean wing Eu	g area flaps ropa XS	<sup>up.</sup> /Classic	: V/N D	iagram	Calcula	ated					AS 0 125	Gust Factor 1 2.78	or 0 125	1 2.87		
5	Based on 2 Cl of 1.67	100 sq ft win clean wing Eu	g area flaps	up. /Classic	: V/N D	liagram	Calcula	ated					AS 0 125	Gust Facto 1 2.78	or 0 125	1 2.87		
5	Based on 2 Cl of 1.67	100 sq ft wing clean wing EU	g area flaps	up.	: V/N D	liagram	Calcula	ated	- -				AS 0 125	Gust Facto	or 0 125	1 2.87		
5	Based on 3 Cl of 1.67	LOO sq ft wing clean wing EU	g area flaps	<sup>up.</sup>	:V/N D	liagram	Calcula	ated					AS 0 125	Gust Facto	or 0 125	1 2.87		
5	Based on 2 Cl of 1.67	100 sq ft win Clean wing Eu	g area flaps Iropa XS	up.	: V/N D	liagram	Calcula	ated					AS 0 125	Gust Facto	or 0 125	1 2.87		
5	Based on : Cl of 1.67 (	LOO sq ft wing Clean wing Eu	g area flaps i	vp. /Classic	v/n d	liagram	Calcula	ated					AS 0 125	Gust Facto	or 0 125	1 2.87		
5	Based on 2 Cl of 1.67	100 sq ft wing Clean wing Eu	g area flaps	up.	v/n d	iagram	Calcula	ated					AS 0 125	Gust Facto	or 0 125	1 2.87		
5 4 L 3	Based on 2 Cl of 1.67 of	LOO sq ft wing Lean wing Eu	g area flaps i	up.	: V/N D	iagram	Calcula	ated					AS 0 125	Gust Facto	or 0 125	1 2.87		
5 4 L 3 0	Based on 1 Cl of 1.67	LOO sq ft wing Clean wing	g area flaps i	up.	: V/N D	iagram	Calcula	ated					AS 0 125	Gust Facto	or 0 125	1 2.87		
L 3 O A	Based on 1 Cl of 1.67	L00 sq ft wing Llean wing	g area flaps	up.	v/n d	iagram	Calcula	ated					AS 0 125	Gust Facto	or 0 125	1 2.87		
L 3 0 A 2 D	Based on 1 Cl of 1.67	L00 sq ft wing Clean wing	g area flaps i	up. /Classic	v/n d	iagram	Calcula	ated	-				AS 0 125	Gust Facto	or 0 125	1 2.87		
L 3 0 A 2 D 2	Based on 1 Cl of 1.67	Eu	g area flaps i	up. /Classic	: V/N D	iagram	Calcula	ated	- 1370				AS 0 125	Gust Facto	or 0 125	1 2.87		
L 3 O A D 2	Based on 1 Cl of 1.67 of	Eu Eu Eu	g area flaps	up.	v/n d	iagram	Calcula	ated	- 1370 - 1430 - 50 (ps gu	st			AS 0 125	Gust Facto	or 0 125 125	1 2.87		
L 3 O A D F 1	Based on 3 Cl of 1.67 of	Eu Eu	g area flaps iropa XS	up.	v/n d	iagram	Calcula	ated	- - - - - - - - - - - - - - - - - - -	st			AS 0 125	Gust Facto	or 0 0 125	1 2.87		
L 3 O A 2 D 2 F 1	Based on 3 Cl of 1.67 of	ECO sq ft win clean wing EU	g area flaps	up.	v/n d	iagram	Calcula	ated	- 1370 - 1370 - 1450 - 50 fps gut - × 66 fps gut	st			AS 0 125	Gust Facto	or 0 0 125	1 2.87		
L 3 0 A 2 D 2 F 1 A C -	Based on 2 Cl of 1.67 of	EUO sq ft win clean wing EU	g area flaps i	up.	v/n d	iagram	Calcula	ated	- 1370 - 1370 - 1450 - 50 (ps gus - ∞ 66 (ps gus	st st			AS 0 125	Gust Facto	or 00 125			
L 3 0 A 2 D 2 F 1 A A C 0	Based on 3 Cl of 1.67 of	LOO sq ft win Llean wing Eu	g area flaps	up.	: V/N D	iagram	Calcula	ated	- - - - - - - - - - - - - - - - - - -	x x x x x x x x x x x x x x x x x x x			AS 0 125	Gust Facto 1 2.78	00 00 125			
L 3 O A 2 F 1 A C 0 T	Based on 3 Cl of 1.67	100 sq ft win Tean wing Eu	g area flaps	vp. //Classic	: V/N D	iiagram	Calcula • • • • • • • • • • • • • • •	ated		t t			AS 0 0 125	Gust Factoria	00 00 125	1 2.87		
L 3 O A 2 D 2 F 1 A A C 0 T	Based on C of 1.67	100 sq ft win Icean wing Eu	g area flaps	/Classic	V/N D	iagram	Calcula a	ated		st t			AS 0 0 125	Gust Factoria	or 0 125	1 2.87		
L 3 O D 2 F 1 A C 0 T O R 1	Based on 1.	100 sq ft winn Itean wing Eu	g area flaps	/Classic	UV/N D	iagram	Calcula 140 2	ated	- - - - - - - - - - - - - - - - - - -	it			AS 0 125	Gust Facture 2,78	or 0 125	1 1 2.87		
L 3 O A 2 D 2 F 1 A C 0 T 0 R 1	Based on 1.07	100 sq ft win Tean wing Eu	g area flaps	/Classic	: <b>V/N D</b>	riagram	Calcula	<b>ated</b>		t t			AS 0 0 125	Gust Factoria	or 0 125 125 125 125 125 125 125 125	1 1 2.87		
L 3 0 A 2 F 1 A 0 T C 0 T C 0 R 1	Based on O	LOO sq ft win itean wing Eu	g area flaps	/Classic	V/N D	iagram	Calcula 140 2	ated	- - - - - - - - - - - - - - - - - - -	i i i i i i i i i i i i i i i i i i i			AS 0 125	Gust Facture 2,78	or 0 125 125 125 125 125 125 125 125	1 1 2.87		
L 3 O D 2 F 1 A C 0 R 1 -2	Based on 1 of 1	100 sq ft win Itean wing Eu	g area flaps	/Classic	: V/N D	iagram	Calcula 140 2	<b>ated</b>	- - - - - - - - - - - - - - - - - - -	x x 1		<	0 0 125	Gust Facture 1 2.78	or 0 125 125 125 125 125 125 125 125	1 1 2.87		
5 4 L 3 0 A 2 F 1 A C 0 T C 0 T C 0 R 1 2 -2	Based on 10 Cl of 167	LOO sq ft wing clean wing Eu	g area flaps	/Classic	• V/N D	riagram	Calcula 	160 11	- - - - - - - - - - - - - - - - - - -	t t 			0 0 125	Gust Facture 1 2.78	or 0 125 125 125 125 125 125 125 125	1 1 2.87		
L 3 0 A 2 F 1 A 0 C 0 T 0 R 1 2 2	Based on O	LOO sq ft win itean wing Eu	g area flaps	/Classic	• V/N D	iagram	Calcula 140 2	ated		it iii iiiiiiiiiiiiiiiiiiiiiiiiiiiiiii			AS 0 0 125	Gust Fatta	or 0 125 125 125 125 125 125 125 125	1 1 2.87		
L 3 O A 2 D 2 F 1 A C 0 T R 1 -2 -3	Based on 1 of 1	100 sq ft win Itean wing Eu	g area flaps	/Classic		iagram		560 11	- - - - - - - - - - - - - - - - - - -	x x i i i i i i i i i i i i i i i i i i			0 0 125	Gust Facture 1 2.78	or 0 125 125 125 125 125 125 125 125			
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Attachment 3

Milb Industrial Kirkbymoorside York Y062 6NR England

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FAX No. \*\* FROM \*\* DATE No. Of Pages \* Dear Stefam Stefan Ridderheim 0046 601 29117 Andy DrAper 22 November, 2000 1 (Including cover page)

The figures rye given you are estimates. which I believe to be realistic, conservative even, Don's figure of 4-5kts is based on the maximum cruise speed, I would expect the differenct to reduce proportionally as aircraft speed was reduced,

Don's comment to me was that the biggest differences you'd notice, as a result of weight increase, would be climb rate and acceleration hence my estimated 50% increase in take-of

The following are my estimates Pon has gone away until mid December), on a 14,301b aircraft, for the remaining cases that you ask for:-

Stall speed (flaps down)S OktsStall speed (flaps up)55ktsFuel consumption (economy) 1 livhr Range<br/>(economy) std tank 600nmR enge (economy) aux tank 90011m

These figures are only estimates: but I believe are as accurate as I can make them. They als are dependent on propeller and standard of build.

I hope that these figures are OK with you.

LII621099700 Kind regards

THARADAIA AHOAUB

Andy Drat



"I echl)ical Manager

Y062 6NR England

B<sup>i</sup>nns IndustAÄl Kirkbymoorside York

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Staffam Ekström - EAA Chapter 22, Sweden

 F.A.O.
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 O046 8751 9816

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 No. Of Pages
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 14 November, 2000

 2 (Including cover page)

Dear Sirs.

Increase in Europa XS gross weight from 1370lb to 1450lb

The Europa XS aircraft and the wings!fuseiage of -5 has been ug,eci in materials in addition to <b>Thus,</b> $3Sg \times i .5 \times ! S^{=}$ A composite factor of ultimate being $3 \ 8 \ x \ 1$ Hence $8.55 =$ 7t42	t has been designed to have a maximum gross weight of i structure Has been tested to \$.35g to qualify it to 3.8g, A consideration of the structure being made using eomposite the normal safety factor of 1.5. <b>8.55g</b> . 13 is •considered acceptable resulting in a test factored .3 = 7.4 lg.	) HEI COFEI		3701b faetor
Therefore 13701b x	15751b*			
However, with consider prudent to limit the max	ration •to the landing gear strength and aircraft performance simum permitted gross weight in Sweden to 14501b,		it	would be
When operating at we from between 58.0 <sup>22</sup> to 6 effects of inertia during	ights above 3701b the centre of gravity limits should be $52.5^{2t}$ aft Of datum (AOD) to between 59.0" to 61 S" (AOL)) ground handling		to	revised reduce
A n <sup>t</sup> h(snugh we have no greater than i 00ft/minu	t demonstrated this, the Europa .XS aircraft at 14501b, when with the RoLax 914 engine and Warp I*ive propeller set to a minimilin static rpm of 5200 conditions, should enable within 300m on a hard uncontaminated n;nway and ite, Kind regards Andy Draper Technical Manager Mills Industrial Kirkbymoorside York V062 6NR England	used in afety 8 x 1 S prudent tween a during e Rotax litions, n	in take-	fitted provide ISA off climb at
111521099900	EUROPALA PADAUE	0002-00		



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Stephane Ridderbeim 0046 6012 9117 Andy Draper 14 November, 2000 2 (Includiug cover page)

Attached is a copy for your reference of the facsimile sent to Staffam Ekström in Sweden, regarding the suggested increase in Europa XS gross weight,

Kind regards

Andy Draper Technicai Manager

S. I spoke to Don Dykins regarding the effect of the extra weight an speed and he estimates Fiskts will be host.